High-Order Methods for Optimization and Control of Conservation Laws on Deforming Domains

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Applied Mathematics Seminar, UC Berkeley Wednesday, September 30, 2015



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Introduction

High-Order Numerical Scheme Fully-Discrete Perturbation Methods Model Order Reduction Conclusion

Questions ...

- How to flap a symmetric, 2D body such that the time-averaged thrust is identically 0?
- Among the kinematically-admissible, zero-thrust flapping motions, which requires the least energy to perform?



Questions ...

- How to flap a symmetric, 2D body such that the time-averaged thrust is identically 0?
- Among the kinematically-admissible, zero-thrust flapping motions, which requires the least energy to perform?

Energy = -9.51	Energy = -0.455	Energy = -1.61
Thrust = 0.198	Thrust = 0.0	Thrust = 0.7



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Harder Question

- What is the energetically-optimal flapping motion of these systems?
- Constraints
 - time-average thrust = 0
 - time-average lift = weight of body and payload
 - stability constraints
 - structural constraints





Micro Aerial Vehicle

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Dragonfly Experiment (A. Song, Brown U)

Harder Question

• What is the optimal shape for each system?









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Time-Dependent PDE-Constrained Optimization

- Optimization of systems that are inherently dynamic or without a steady-state solution
- Optimal control of body immersed in a fluid
 - Goal: Determine **kinematics** that minimizes a cost functional, subject to constraints
- Shape optimization of body in turbulent flow
 - Goal: Determine **shape** that minimizes a cost functional, subject to constraints



Micro Aerial Vehicle



Vertical Windmill







Introduction

High-Order Numerical Scheme Fully-Discrete Perturbation Methods Model Order Reduction Conclusion

• $\mathcal{J}(\boldsymbol{U},\boldsymbol{\mu}) = \int_{T_0}^{T_f} \int_{\boldsymbol{\Gamma}} j(\boldsymbol{U},\boldsymbol{\mu},t) \, dS \, dt$

• $C(U, \mu) = \int_{T_0}^{T_f} \int_{\Gamma} c(U, \mu, t) \, dS \, dt$

Problem Formulation

Goal: Find the solution of the unsteady PDE-constrained optimization problem

$$\begin{array}{ll} \underset{\boldsymbol{U},\ \boldsymbol{\mu}}{\text{minimize}} & \mathcal{J}(\boldsymbol{U},\boldsymbol{\mu}) \\ \text{subject to} & \boldsymbol{C}(\boldsymbol{U},\boldsymbol{\mu}) \leq 0 \\ & \frac{\partial \boldsymbol{U}}{\partial t} + \nabla \cdot \boldsymbol{F}(\boldsymbol{U},\nabla \boldsymbol{U}) = 0 \ \text{ in } \ v(\boldsymbol{\mu},t) \end{array}$$

where

• μ

• $\boldsymbol{U}(\boldsymbol{x},t)$

PDE solution design/control parameters

objective function

H N

constraints





ALE Description of Conservation Law

- Introduce map from fixed reference domain V to physical, deformable (parametrized) domain $v(\pmb{\mu},t)$
- A point $X \in V$ is mapped to $x(\mu, t) = \mathcal{G}(\mathbf{X}, \mu, t) \in v(\mu, t)$







Spatial Discretization: Discontinuous Galerkin

• Re-write conservation law as first-order system

$$\left. \frac{\partial \boldsymbol{U}_{\boldsymbol{X}}}{\partial t} \right|_{\boldsymbol{X}} + \nabla_{\boldsymbol{X}} \cdot \boldsymbol{F}_{\boldsymbol{X}}(\boldsymbol{U}_{\boldsymbol{X}}, \ \boldsymbol{Q}_{\boldsymbol{X}}) = \boldsymbol{0}$$
$$\boldsymbol{Q}_{\boldsymbol{X}} - \nabla_{\boldsymbol{X}} \boldsymbol{U}_{\boldsymbol{X}} = \boldsymbol{0}$$

• Discretize using DG

- Roe's method for inviscid flux
- Compact DG (CDG) for viscous flux
- *Semi-discrete* equations

$$\mathbb{M}\frac{\partial \boldsymbol{u}}{\partial t} = \boldsymbol{r}(\boldsymbol{u}, \boldsymbol{\mu}, t)$$
$$\boldsymbol{u}(0) = \boldsymbol{u}_0(\boldsymbol{\mu})$$

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Stencil for CDG, LDG, and BR2 fluxes





Temporal Discretization: Diagonally-Implicit Runge-Kutta

- Diagonally-Implicit RK (DIRK) are implicit Runge-Kutta schemes defined by lower triangular Butcher tableau → **decoupled implicit stages**
- Overcomes issues with high-order BDF and IRK
 - Limited accuracy of A-stable BDF schemes (2nd order)
 - High cost of general implicit RK schemes (coupled stages)

$$u^{(0)} = u_0(\mu)$$

$$u^{(n)} = u^{(n-1)} + \sum_{i=1}^{s} b_i k_i^{(n)}$$

$$u_i^{(n)} = u^{(n-1)} + \sum_{j=1}^{i} a_{ij} k_j^{(n)}$$

$$\mathbb{M}k_i^{(n)} = \Delta t_n r \left(u_i^{(n)}, \ \mu, \ t_{n-1} + c_i \Delta t_n \right)$$

c_1	a_{11}			
c_2	a_{21}	a_{22}		
÷	:	÷	·	
c_s	a_{s1}	a_{s2}	•••	a_{ss}
	b_1	b_2	•••	b_s

Butcher Tableau for DIRK scheme





Globally High-Order Discretization

• Fully-Discrete Conservation Law

$$u^{(0)} = u_0(\mu)$$

$$u^{(n)} = u^{(n-1)} + \sum_{i=1}^{s} b_i k_i^{(n)}$$

$$u_i^{(n)} = u^{(n-1)} + \sum_{j=1}^{i} a_{ij} k_j^{(n)}$$

$$\mathbb{M}k_i^{(n)} = \Delta t_n r \left(u_i^{(n)}, \ \mu, \ t_{n-1} + c_i \Delta t_n \right)$$

• Fully-Discrete Output Functional

$$F(u^{(0)},\ldots,u^{(N_t)},k_1^{(1)},\ldots,k_s^{(N_t)},\mu)$$



ESG

Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

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Adjoint Method for PDE-Constrained Optimization

• Continuous PDE-constrained optimization problem

$$\begin{array}{ll} \underset{\boldsymbol{U}, \ \boldsymbol{\mu}}{\text{minimize}} & \mathcal{J}(\boldsymbol{U}, \boldsymbol{\mu}) \\ \text{subject to} & \boldsymbol{C}(\boldsymbol{U}, \boldsymbol{\mu}) \leq 0 \\ & \frac{\partial \boldsymbol{U}}{\partial t} + \nabla \cdot \boldsymbol{F}(\boldsymbol{U}, \nabla \boldsymbol{U}) = 0 \ \text{ in } \ v(\boldsymbol{\mu}, t) \end{array}$$

• Replace conservation law and functional with fully-discrete high-order numerical approximation



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Adjoint Method for PDE-Constrained Optimization

• Fully-discrete PDE-constrained optimization problem



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Generalized Reduced-Gradient Approach

OPTIMIZER

MESH MOTION





Zahr, Persson, Farhat Optimization/Control Conservation Laws



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Generalized Reduced-Gradient Approach

PRIMAL PDE

OPTIMIZER

MESH MOTION







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Generalized Reduced-Gradient Approach

PRIMAL PDE









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Generalized Reduced-Gradient Approach





DUAL PDE



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Adjoint Method

- Consider the fully-discrete output functional $F(\boldsymbol{u}^{(n)}, \boldsymbol{k}^{(n)}_i, \boldsymbol{\mu})$
 - Represents either the **objective** function or a **constraint**
- The *total derivative* with respect to the parameters μ , required in the context of gradient-based optimization, takes the form

$$\frac{\mathrm{d}F}{\mathrm{d}\boldsymbol{\mu}} = \frac{\partial F}{\partial \boldsymbol{\mu}} + \sum_{n=0}^{N_t} \frac{\partial F}{\partial \boldsymbol{u}^{(n)}} \frac{\partial \boldsymbol{u}^{(n)}}{\partial \boldsymbol{\mu}} + \sum_{n=1}^{N_t} \sum_{i=1}^s \frac{\partial F}{\partial \boldsymbol{k}_i^{(n)}} \frac{\partial \boldsymbol{k}_i^{(n)}}{\partial \boldsymbol{\mu}}$$

- The sensitivities, $\frac{\partial \boldsymbol{u}^{(n)}}{\partial \mu}$ and $\frac{\partial \boldsymbol{k}_i^{(n)}}{\partial \mu}$, are expensive to compute, requiring the solution of n_{μ} linear evolution equations
- Adjoint method: alternative method for computing $\frac{dF}{d\mu}$ requiring one linear evolution evoluation equation for each output functional, F



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Overview of Adjoint Derivation

• Define **auxiliary** PDE-constrained optimization problem

$$\begin{array}{l} \underset{\boldsymbol{u}^{(0)}}{\text{minimize}} & F(\boldsymbol{u}^{(0)}, \ \dots, \ \boldsymbol{u}^{(N_t)}, \ \boldsymbol{k}_1^{(1)}, \ \dots, \ \boldsymbol{k}_s^{(N_t)}, \ \bar{\boldsymbol{\mu}}) \\ \\ \boldsymbol{k}_1^{(1)}, \ \dots, \ \boldsymbol{k}_s^{(N_t)} \in \mathbb{R}^{N_{\boldsymbol{u}}} & \\ \end{array} \\ \text{subject to} & \tilde{\boldsymbol{r}}^{(0)} = \boldsymbol{u}^{(0)} - \boldsymbol{u}_0(\bar{\boldsymbol{\mu}}) = 0 \\ \\ & \tilde{\boldsymbol{r}}^{(n)} = \boldsymbol{u}^{(n)} - \boldsymbol{u}^{(n-1)} + \sum_{i=1}^s b_i \boldsymbol{k}_i^{(n)} = 0 \\ & \boldsymbol{R}_i^{(n)} = \mathbb{M} \boldsymbol{k}_i^{(n)} - \Delta t_n \boldsymbol{r} \left(\boldsymbol{u}_i^{(n)}, \ \bar{\boldsymbol{\mu}}, \ t_i^{(n-1)} \right) = 0 \end{array}$$

• Define Lagrangian

$$\mathcal{L}(\boldsymbol{u}^{(n)}, \, \boldsymbol{k}_{i}^{(n)}, \, \boldsymbol{\lambda}^{(n)}, \, \boldsymbol{\kappa}_{i}^{(n)}) = F - \boldsymbol{\lambda}^{(0)}{}^{T} \tilde{\boldsymbol{r}}^{(0)} - \sum_{n=1}^{N_{t}} \boldsymbol{\lambda}^{(n)}{}^{T} \tilde{\boldsymbol{r}}^{(n)} - \sum_{n=1}^{N_{t}} \sum_{i=1}^{s} \boldsymbol{\kappa}_{i}^{(n)}{}^{T} \boldsymbol{R}_{i}^{(n)}$$



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Fully-Discrete Adjoint Equations

• The solution of the optimization problem is given by the Karush-Kuhn-Tucker (KKT) sytem

$$\frac{\partial \mathcal{L}}{\partial \boldsymbol{u}^{(n)}} = 0, \quad \frac{\partial \mathcal{L}}{\partial \boldsymbol{k}_i^{(n)}} = 0, \quad \frac{\partial \mathcal{L}}{\partial \boldsymbol{\lambda}^{(n)}} = 0, \quad \frac{\partial \mathcal{L}}{\partial \boldsymbol{\kappa}_i^{(n)}} = 0$$

• The derivatives w.r.t. the state variables, $\frac{\partial \mathcal{L}}{\partial u^{(n)}} = 0$ and $\frac{\partial \mathcal{L}}{\partial k_i^{(n)}} = 0$, yield the fully-discrete adjoint equations

$$\boldsymbol{\lambda}^{(N_t)} = \frac{\partial F}{\partial \boldsymbol{u}^{(N_t)}}^T$$
$$\boldsymbol{\lambda}^{(n-1)} = \boldsymbol{\lambda}^{(n)} + \frac{\partial F}{\partial \boldsymbol{u}^{(n-1)}}^T + \sum_{i=1}^s \Delta t_n \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{u}} \left(\boldsymbol{u}_i^{(n)}, \ \boldsymbol{\mu}, \ t_{n-1} + c_i \Delta t_n \right)^T \boldsymbol{\kappa}_i^{(n)}$$
$$\mathbb{M}^T \boldsymbol{\kappa}_i^{(n)} = \frac{\partial F}{\partial \boldsymbol{u}^{(N_t)}}^T + b_i \boldsymbol{\lambda}^{(n)} + \sum_{j=i}^s a_{ji} \Delta t_n \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{u}} \left(\boldsymbol{u}_j^{(n)}, \ \boldsymbol{\mu}, \ t_{n-1} + c_j \Delta t_n \right)^T \boldsymbol{\kappa}_i^{(n)}$$



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Fully-Discrete Adjoint Equations: Dissection

$$\boldsymbol{\lambda}^{(N_t)} = \frac{\partial F}{\partial \boldsymbol{u}^{(N_t)}}^T$$
$$\boldsymbol{\lambda}^{(n-1)} = \boldsymbol{\lambda}^{(n)} + \frac{\partial F}{\partial \boldsymbol{u}^{(n-1)}}^T + \sum_{i=1}^s \Delta t_n \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{u}} \left(\boldsymbol{u}_i^{(n)}, \ \boldsymbol{\mu}, \ t_{n-1} + c_i \Delta t_n \right)^T \boldsymbol{\kappa}_i^{(n)}$$
$$\mathbb{M}^T \boldsymbol{\kappa}_i^{(n)} = \frac{\partial F}{\partial \boldsymbol{u}^{(N_t)}}^T + b_i \boldsymbol{\lambda}^{(n)} + \sum_{j=i}^s a_{ji} \Delta t_n \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{u}} \left(\boldsymbol{u}_j^{(n)}, \ \boldsymbol{\mu}, \ t_{n-1} + c_j \Delta t_n \right)^T \boldsymbol{\kappa}_j^{(n)}$$

- Linear evolution equations solved backward in time
 - Requires solving linear systems of equations with $\frac{\partial r}{\partial x}^{T}$
 - Accurate solution of linear system required
- $\bullet\,$ Primal state, $m{u}^{(n)},$ and stage, $m{k}^{(n)}_i,$ required at each state/stage of dual solve
 - Parallel I/O



- Heavily-dependent on **chosen ouput**
 - $\boldsymbol{\lambda}^{(n)}$ and $\boldsymbol{\kappa}^{(n)}_i$ must be computed for each output functional F



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Gradient Reconstruction via Dual Variables

• Equipped with the solution to the primal problem, $\boldsymbol{u}^{(n)}$ and $\boldsymbol{k}_i^{(n)}$, and dual problem, $\boldsymbol{\lambda}^{(n)}$ and $\boldsymbol{\kappa}_i^{(n)}$, the output gradient is reconstructed as

$$\frac{\mathrm{d}F}{\mathrm{d}\mu} = \frac{\partial F}{\partial \mu} - \boldsymbol{\lambda}^{(0)T} \frac{\partial \boldsymbol{u}_0}{\partial \mu} - \sum_{n=1}^{N_t} \Delta t_n \sum_{i=1}^s \boldsymbol{\kappa}_i^{(n)T} \frac{\partial \boldsymbol{r}}{\partial \mu} (\boldsymbol{u}_i^{(n)}, \ \boldsymbol{\mu}, \ t_i^{(n)})$$
• Independent of sensitivities, $\frac{\partial \boldsymbol{u}^{(n)}}{\partial \mu}$ and $\frac{\partial \boldsymbol{k}_i^{(n)}}{\partial \mu}$





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Shape Optimization

• Recall formula for reconstruction output gradient from primal/dual variables

$$\frac{\mathrm{d}F}{\mathrm{d}\boldsymbol{\mu}} = \frac{\partial F}{\partial \boldsymbol{\mu}} - \boldsymbol{\lambda}^{(0)T} \frac{\partial \boldsymbol{u}_0}{\partial \boldsymbol{\mu}} - \sum_{n=1}^{N_t} \Delta t_n \sum_{i=1}^s \boldsymbol{\kappa}_i^{(n)T} \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{\mu}} (\boldsymbol{u}_i^{(n)}, \ \boldsymbol{\mu}, \ t_i^{(n)})$$

- Dependence on sensitivity of initial condition, $\frac{\partial u_0}{\partial \mu}$
 - Non-zero if $u_0(\mu)$ is *steady-state* for a μ -parametrized shape
 - $\frac{\partial u_0}{\partial \mu}$ computed via standard sensitivity analysis for steady-state problems OR
 - $\lambda^{(0)T} \frac{\partial u_0}{\partial \mu}$ computed directly via standard adjoint method for steady-state problems
- This complication is circumvented in this work by choosing a zero freestream $\implies u_0(\mu) = 0$





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Problem Setup

$$\begin{array}{ll} \underset{\boldsymbol{w}}{\text{maximize}} & \int_{0}^{T} \int_{\boldsymbol{\Gamma}} \boldsymbol{f} \cdot \boldsymbol{v} \, dS \, dt \\ \text{subject to} & \frac{\partial \boldsymbol{U}}{\partial t} + \nabla \cdot \boldsymbol{F}(\boldsymbol{U}, \nabla \boldsymbol{U}) = 0 \end{array}$$



Airfoil schematic, kinematic description

• Radial basis function parametrization

$$oldsymbol{X}' = oldsymbol{X} + \sum oldsymbol{w}_i \Phi(||oldsymbol{X} - oldsymbol{c}_i||)$$

- Zero freestream velocity
- $h(t), \theta(t)$ prescribed
- Black-box optimizer: SNOPT



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Optimization Results: Vorticity Field History

- Initial guess
 - $h_0(t), \theta_0(t)$ prescribed
 - **w** = **0**

- Optimization 1
 - $h_0(t), \theta_0(t)$ prescribed
 - \boldsymbol{w} variable









Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Optimization Summary

	$\int F_x dt$	$\int F_y dt$	$\int T_z dt$	$\int F_y \cdot \dot{h} dt$	$-\int T_z \cdot \dot{\theta} dt$	$\int \boldsymbol{f} \cdot \boldsymbol{v} dt$
Initial	-0.634	-0.727	-0.138	-0.526	-0.484	-1.01
Optimal	-0.461	-0.959	-0.183	-0.145	-0.465	-0.609





Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Problem Setup

 $\underset{h(t),\theta(t)}{\text{maximize}}$

$$J_0 \quad J_{\mathbf{\Gamma}} \quad h(0) = h'(0) = h'(T) = 0, \ h(T) = 1$$
$$\theta(0) = \theta'(0) = \theta(T) = \theta'(T) = 0$$
$$\frac{\partial \mathbf{U}}{\partial t} + \nabla \cdot \mathbf{F}(\mathbf{U}, \nabla \mathbf{U}) = 0$$



Airfoil schematic, kinematic description

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- Non-zero freestream velocity
- $h(t), \theta(t)$ discretized via *clamped cubic splines*
- Knots of cubic splines as optimization parameters, μ

 $\int_{-\infty}^{T} \int \mathbf{f} \cdot \mathbf{v} \, dS \, dt$



Black-box optimizer: SNOPT

Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Optimization Setup

- $\bullet~$ Initial guess (- -)
 - $h(t) = h_0(t) = (1 \cos(\pi t/T))/2$
 - $\theta(t) = \theta_0(t) = 0$
- Optimization 1 (-----)
 - $h(t) = (1 \cos(\pi t/T))/2$
 - $\theta(t)$ parametrized (clamped cubic splines)
- Optimization 2 (-----)
 - $h(t), \theta(t)$ parametrized (clamped cubic splines)





Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Optimization Results: Vorticity Field History

Energy = -1.47

Energy = -0.120

Energy = 0.756



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Optimization Summary

	$\int F_x dt$	$\int F_y dt$	$\int T_z dt$	$\int F_y \cdot \dot{h} dt$	$-\int T_z \cdot \dot{\theta} dt$	$\int \boldsymbol{f} \cdot \boldsymbol{v} dt$
()	-0.121	-2.41	0.0123	-1.47	0.00	-1.47
()	0.978	0.872	-0.107	0.585	-0.705	-0.120
()	3.34	2.54	2.59	1.56	-0.804	0.756





Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Problem Setup

$$\begin{array}{ll} \underset{h(t),\theta(t)}{\text{maximize}} & \int_{0}^{T} \int_{\Gamma} \boldsymbol{f} \cdot \boldsymbol{v} \, dS \, dt \\ \text{subject to} & -\int_{0}^{T} \int_{\Gamma} F_{x} \, dS \, dt \geq c \\ & h^{(k)}(t) = h^{(k)}(t+T) \\ & \theta^{(k)}(t) = \theta^{(k)}(t+T) \\ & \frac{\partial \boldsymbol{U}}{\partial t} + \nabla \cdot \boldsymbol{F}(\boldsymbol{U}, \nabla \boldsymbol{U}) = \end{array}$$



Airfoil schematic, kinematic description

- Non-zero freestream velocity
- $h(t), \theta(t)$ discretized via phase/amplitude of Fourier modes
- Knots of cubic splines as optimization

parameters, μ



Black-box optimizer: SNOPT



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Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Optimization Setup

- Initial guess (---)
 - $h(t) = -\cos(0.4\pi t/T)$
 - $\theta(t) = 0$
- Optimization 1 (-----)
 - c = 0.0
 - $h(t), \theta(t)$ parametrized (Fourier)
- Optimization 2 (-----)
 - c = 0.3
 - $h(t), \theta(t)$ parametrized (Fourier)

- Optimization 3 (-----)
 - c = 0.5
 - $h(t), \theta(t)$ parametrized (Fourier)
- Optimization 4 (-----)
 - c = 0.7
 - $h(t), \theta(t)$ parametrized (Fourier)





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Optimization Results: Vorticity Field History

Energy = -9.51	
Thrust $= 0.198$	

Energy = -0.455Thrust = 0.0

Energy = -1.61Thrust = 0.7



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Optimization Summary

	$\int F_x dt$	$\int F_y dt$	$\int T_z dt$	$\int F_y \cdot \dot{h} dt$	$-\int T_z \cdot \dot{\theta} dt$	$\int \boldsymbol{f} \cdot \boldsymbol{v} dt$
Initial ()	-0.198	-0.0447	-0.0172	-9.51	0.0	-9.51
c = 0.0 ()	0.0	0.0142	0.0	-0.425	-0.0303	-0.455
c = 0.3 ()	-0.3	0.0245	0.00319	-0.894	-0.0459	-0.940
c = 0.5 ()	-0.5	0.0319	0.00501	-1.22	-0.0557	-1.27
c = 0.7 ()	-0.7	0.0510	0.00897	-1.55	-0.0650	-1.61





Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Time-Periodic Solutions

- To properly optimize a cyclic, or periodic problem, need to simulate a **representative** period
- Necessary to avoid transients that will impact output functionals
- Task: Find initial condition, u_0 , such that flow is periodic, i.e. $u^{(N_t)} = u_0$



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Fully-Discrete Time-Periodic Solution

• Recall fully-discrete conservation law

$$u^{(0)} = u_0(\mu)$$

$$u^{(n)} = u^{(n-1)} + \sum_{i=1}^{s} b_i k_i^{(n)}$$

$$u_i^{(n)} = u^{(n-1)} + \sum_{j=1}^{i} a_{ij} k_j^{(n)}$$

$$\mathbb{M}k_i^{(n)} = \Delta t_n r \left(u_i^{(n)}, \ \mu, \ t_{n-1} + c_i \Delta t_n \right)$$

• Time-periodicity is defined as

$$\boldsymbol{u}^{(N_t)}(\boldsymbol{u}_0) = \boldsymbol{u}_0$$





Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Shooting Method for Time-Periodic Solutions

• Apply Newton's method to solve nonlinear system of equations

$$\boldsymbol{R}(\boldsymbol{u}_0) = \boldsymbol{u}^{(N_t)}(\boldsymbol{u}_0) - \boldsymbol{u}_0 = 0$$

• Nonlinear iteration defined as

$$\boldsymbol{u}_0 \leftarrow \boldsymbol{u}_0 - \boldsymbol{J}(\boldsymbol{u}_0)^{-1} \boldsymbol{R}(\boldsymbol{u}_0)$$

where
$$oldsymbol{J}(oldsymbol{u}_0) = rac{\partialoldsymbol{u}^{(N_t)}}{\partialoldsymbol{u}_0} - oldsymbol{I}$$

• $\frac{\partial \boldsymbol{u}^{(N_t)}}{\partial \boldsymbol{u}_0}$ is a large, dense matrix and expensive to construct

• Krylov method to solve $\boldsymbol{J}(\boldsymbol{u}_0)^{-1} \boldsymbol{R}(\boldsymbol{u}_0)$ only requires matrix-vector products



$$oldsymbol{J}(oldsymbol{u}_0)oldsymbol{v} = rac{\partialoldsymbol{u}^{(N_t)}}{\partialoldsymbol{u}_0}oldsymbol{v} - oldsymbol{v}$$



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Fully-Discrete Sensitivity Method

• Direct differentiation of fully-discrete conservation law, and multiplication by $\boldsymbol{v},$ leads to the fully-discrete sensitivity equations

$$\begin{split} &\frac{\partial \boldsymbol{u}^{(0)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} = \boldsymbol{v} \\ &\frac{\partial \boldsymbol{u}^{(n)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} = \frac{\partial \boldsymbol{u}^{(n-1)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} + \sum_{i=1}^s b_i \frac{\partial \boldsymbol{k}_i^{(n)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} \\ &\mathbb{M} \frac{\partial \boldsymbol{k}_i^{(n)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} = \Delta t_n \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{u}} \left(\boldsymbol{u}_i^{(n)}, \ \boldsymbol{\mu}, \ t_i^{(n-1)} \right) \left[\frac{\partial \boldsymbol{u}^{(n-1)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} + \sum_{j=1}^i a_{ij} \frac{\partial \boldsymbol{k}_j^{(n)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} \right] \end{split}$$

• Sensitivity variables: $\frac{\partial \boldsymbol{u}^{(n)}}{\partial \boldsymbol{u}_0} \boldsymbol{v}$, and $\frac{\partial \boldsymbol{k}_i^{(n)}}{\partial \boldsymbol{u}_0} \boldsymbol{v}$



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

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Fully-Discrete Sensitivity Equations: Dissection

$$\begin{aligned} &\frac{\partial \boldsymbol{u}^{(0)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} = \boldsymbol{v} \\ &\frac{\partial \boldsymbol{u}^{(n)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} = \frac{\partial \boldsymbol{u}^{(n-1)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} + \sum_{i=1}^s b_i \frac{\partial \boldsymbol{k}^{(n)}_i}{\partial \boldsymbol{u}_0} \boldsymbol{v} \\ &\mathbb{M} \frac{\partial \boldsymbol{k}^{(n)}_i}{\partial \boldsymbol{u}_0} \boldsymbol{v} = \Delta t_n \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{u}} \left(\boldsymbol{u}^{(n)}_i, \ \boldsymbol{\mu}, \ t^{(n-1)}_i \right) \left[\frac{\partial \boldsymbol{u}^{(n-1)}}{\partial \boldsymbol{u}_0} \boldsymbol{v} + \sum_{j=1}^i a_{ij} \frac{\partial \boldsymbol{k}^{(n)}_j}{\partial \boldsymbol{u}_0} \boldsymbol{v} \right] \end{aligned}$$

- $\bullet\,$ Linear evolution equations solved forward in time for each v
 - Requires solving linear systems of equations with $\frac{\partial r}{\partial u}$
 - Accurate solution of linear system required
- Primal state, $\pmb{u}^{(n)},$ and stage, $\pmb{k}_i^{(n)},$ required at each state/stage of sensitivity solve



Problem Setup

Find \boldsymbol{u}_0 such that

$$\boldsymbol{R}(\boldsymbol{u}_0) = \boldsymbol{u}^{(N_t)}(\boldsymbol{u}_0) - \boldsymbol{u}_0 = 0$$

and $\boldsymbol{u}^{(N_t)}$ is the solution of the fully-discrete conservation law at the final time step, N_t



Sensitivity Method for Time-Periodic Solutions

Airfoil schematic, kinematic description

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- $h(t), \theta(t)$ prescribed
- Nonlinear solvers
 - Fixed-point iteration
 - Newton-Raphson method
- Linear solver: Unpreconditioned GMRES
- Fully-discrete sensitivity method used to



compute
$$rac{\partial oldsymbol{u}^{(N_t)}}{\partial oldsymbol{u}_0}oldsymbol{v}$$

Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Time-Periodic Flow: Flapping Foil

Initial Guess for Newton-Krylov Steady-State Flow



Solution of Newton-Krylov





Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Nonlinear Solver Convergence



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Linear Solver Convergence



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

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Periodic PDE-Constrained Optimization

Recall fully-discrete PDE-constrained optimization problem

$$\begin{array}{l} \underset{\boldsymbol{u}^{(0)}, \dots, \boldsymbol{u}^{(N_t)} \in \mathbb{R}^{N_u}, \\ \boldsymbol{k}_1^{(1)}, \dots, \boldsymbol{k}_s^{(N_t)} \in \mathbb{R}^{N_u}, \\ \boldsymbol{\mu} \in \mathbb{R}^{n_\mu} \end{array} & J(\boldsymbol{u}^{(0)}, \dots, \boldsymbol{u}^{(N_t)}, \boldsymbol{k}_1^{(1)}, \dots, \boldsymbol{k}_s^{(N_t)}, \boldsymbol{\mu}) \\ \text{subject to} & \mathbf{C}(\boldsymbol{u}^{(0)}, \dots, \boldsymbol{u}^{(N_t)}, \boldsymbol{k}_1^{(1)}, \dots, \boldsymbol{k}_s^{(N_t)}, \boldsymbol{\mu}) \leq 0 \\ & \boldsymbol{u}^{(0)} - \boldsymbol{u}_0(\boldsymbol{\mu}) = 0 \\ & \boldsymbol{u}^{(n)} - \boldsymbol{u}^{(n-1)} + \sum_{i=1}^s b_i \boldsymbol{k}_i^{(n)} = 0 \\ & \mathbb{M} \boldsymbol{k}_i^{(n)} - \Delta t_n \boldsymbol{r} \left(\boldsymbol{u}_i^{(n)}, \boldsymbol{\mu}, t_i^{(n-1)} \right) = 0 \end{array}$$





Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Periodic PDE-Constrained Optimization

Slight modification leads to fully-discrete periodic PDE-constrained optimization problem

$$\begin{array}{l} \underset{\boldsymbol{u}^{(0)}, \dots, \, \boldsymbol{u}^{(N_t)} \in \mathbb{R}^{N_{\boldsymbol{u}}}, \\ \boldsymbol{k}_1^{(1)}, \dots, \, \boldsymbol{k}_s^{(N_t)} \in \mathbb{R}^{N_{\boldsymbol{u}}}, \\ \boldsymbol{\mu} \in \mathbb{R}^{n_{\boldsymbol{\mu}}} \end{array} & J(\boldsymbol{u}^{(0)}, \, \dots, \, \boldsymbol{u}^{(N_t)}, \, \boldsymbol{k}_1^{(1)}, \, \dots, \, \boldsymbol{k}_s^{(N_t)}, \, \boldsymbol{\mu}) \\ \text{subject to} & \mathbf{C}(\boldsymbol{u}^{(0)}, \, \dots, \, \boldsymbol{u}^{(N_t)}, \, \boldsymbol{k}_1^{(1)}, \, \dots, \, \boldsymbol{k}_s^{(N_t)}, \, \boldsymbol{\mu}) \leq 0 \\ & \boldsymbol{u}^{(0)} - \boldsymbol{u}^{(N_t)} = 0 \\ & \boldsymbol{u}^{(n)} - \boldsymbol{u}^{(n-1)} + \sum_{i=1}^s b_i \boldsymbol{k}_i^{(n)} = 0 \\ & \mathbb{M} \boldsymbol{k}_i^{(n)} - \Delta t_n \boldsymbol{r} \left(\boldsymbol{u}_i^{(n)}, \, \boldsymbol{\mu}, \, t_i^{(n-1)} \right) = 0 \end{array}$$



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Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

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Adjoint Method for Periodic PDE-Constrained Optimization

• Following identical procedure as for non-periodic case, the adjoint equations corresponding to the periodic conservation law are

$$\boldsymbol{\lambda}^{(N_t)} = \boldsymbol{\lambda}^{(0)} + \frac{\partial F}{\partial \boldsymbol{u}^{(N_t)}}^T$$
$$\boldsymbol{\lambda}^{(n-1)} = \boldsymbol{\lambda}^{(n)} + \frac{\partial F}{\partial \boldsymbol{u}^{(n-1)}}^T + \sum_{i=1}^s \Delta t_n \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{u}} \left(\boldsymbol{u}_i^{(n)}, \ \boldsymbol{\mu}, \ t_{n-1} + c_i \Delta t_n \right)^T \boldsymbol{\kappa}_i^{(n)}$$
$$\mathbb{M}^T \boldsymbol{\kappa}_i^{(n)} = \frac{\partial F}{\partial \boldsymbol{u}^{(N_t)}}^T + b_i \boldsymbol{\lambda}^{(n)} + \sum_{j=i}^s a_{ji} \Delta t_n \frac{\partial \boldsymbol{r}}{\partial \boldsymbol{u}} \left(\boldsymbol{u}_j^{(n)}, \ \boldsymbol{\mu}, \ t_{n-1} + c_j \Delta t_n \right)^T \boldsymbol{\kappa}_j^{(n)}$$

- Dual problem is also periodic
- Solve *linear, periodic* problem using Krylov shooting method



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Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Generalized Reduced-Gradient Approach



Adjoint Method for PDE-Constrained Optimization Sensitivity Method for Time-Periodic Solutions Adjoint Method with Periodicity Constraint

Overview

- Utilized high-order DG-DIRK discretization of general conservation laws with a mapping-based ALE formulation for deforming domains
- Introduced fully-discrete adjoint method for computing gradients of output functionals
 - Framework demonstrated on the computation of energetically-optimal motions of a 2D airfoil in a flow field with constraints
- Introduced fully-discrete sensitivity equations and used Newton-Krylov shooting method to compute time-periodic flows
- Next steps: periodic optimization, 3D, multiphysics, model reduction



Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Problem Formulation

Goal: Rapidly solve PDE-constrained optimization problems of the form

 $\begin{array}{ll} \underset{\boldsymbol{u} \in \mathbb{R}^{N_{\boldsymbol{u}}}, \ \boldsymbol{\mu} \in \mathbb{R}^{n_{\boldsymbol{\mu}}}}{\text{minimize}} & f(\boldsymbol{u}, \boldsymbol{\mu}) \\ \text{subject to} & \boldsymbol{R}(\boldsymbol{u}, \boldsymbol{\mu}) = 0 \end{array}$

where $\mathbf{R} : \mathbb{R}^{N_{u}} \times \mathbb{R}^{n_{\mu}} \to \mathbb{R}^{N_{u}}$ is the discretized (steady, nonlinear) PDE, u is the PDE state vector, μ is the vector of parameters, and N_{u} is assumed to be very large.



Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Reduced-Order Model

• Model Order Reduction (MOR) assumption: *state vector lies in low-dimensional subspace*

$$oldsymbol{u}pproxoldsymbol{u}_r=oldsymbol{\Phi}oldsymbol{y} \qquad \Longrightarrow \qquad rac{\partialoldsymbol{u}}{\partialoldsymbol{\mu}}pproxrac{\partialoldsymbol{u}_r}{\partialoldsymbol{\mu}}=oldsymbol{\Phi}rac{\partialoldsymbol{y}}{\partialoldsymbol{\mu}}$$

where $\boldsymbol{y} \in \mathbb{R}^{n_{\boldsymbol{y}}}$ are the reduced coordinates of \boldsymbol{u}_r in the basis $\boldsymbol{\Phi} \in \mathbb{R}^{N_{\boldsymbol{u}} \times n_{\boldsymbol{y}}}$, and $n_{\boldsymbol{y}} \ll N_{\boldsymbol{u}}$

• Substitute assumption into High-Dimensional Model (HDM), ${m R}({m u},{m \mu})=0$

$$\boldsymbol{R}(\boldsymbol{\Phi}\boldsymbol{y},\boldsymbol{\mu}) \approx 0$$

• Require projection of residual in low-dimensional left subspace, with basis $\Psi \in \mathbb{R}^{N_u \times n_y}$ to be zero

$$\boldsymbol{R}_r(\boldsymbol{y},\boldsymbol{\mu}) = \boldsymbol{\Psi}^T \boldsymbol{R}(\boldsymbol{\Phi} \boldsymbol{y},\boldsymbol{\mu}) = \boldsymbol{0}$$



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Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Definition of Φ : Proper Orthogonal Decomposition

• Perfect basis should satisify:

$$\{ oldsymbol{u}(oldsymbol{\mu}) \} \; igcup \; \left\{ rac{\partial oldsymbol{u}}{\partial oldsymbol{\mu}}(oldsymbol{\mu})
ight\} \subseteq ext{range } oldsymbol{\Phi}$$

State-Sensitivity POD

• Collect state and sensitivity snapshots by sampling HDM

$$egin{aligned} oldsymbol{X} &= egin{bmatrix} oldsymbol{u}(oldsymbol{\mu}_1) & oldsymbol{u}(oldsymbol{\mu}_2) & \cdots & oldsymbol{u}(oldsymbol{\mu}_n) \end{bmatrix} \ oldsymbol{Y} &= egin{bmatrix} rac{\partialoldsymbol{u}}{\partialoldsymbol{\mu}}(oldsymbol{\mu}_1) & rac{\partialoldsymbol{u}}{\partialoldsymbol{\mu}}(oldsymbol{\mu}_2) & \cdots & rac{\partialoldsymbol{u}}{\partialoldsymbol{\mu}}(oldsymbol{\mu}_n) \end{bmatrix} \end{aligned}$$

• Use Proper Orthogonal Decomposition to generate reduced bases from each *individually*, and concatenate to get ROB



$$\boldsymbol{\Phi} = \begin{bmatrix} \text{POD}(\boldsymbol{X}) & \text{POD}(\boldsymbol{Y}) \end{bmatrix}$$

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Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Definition of Ψ : Minimum-Residual ROM

- Recall ROM governing equation: $\boldsymbol{R}_r(\boldsymbol{y},\ \boldsymbol{\mu}) \equiv \boldsymbol{\Psi}^T \boldsymbol{R}(\boldsymbol{\Phi} \boldsymbol{y},\ \boldsymbol{\mu}) = 0$
- $\bullet\,$ Standard options for choice of left basis $\Psi\,$
 - Galerkin: $\Psi = \Phi$
 - Least-Squares Petrov-Galerkin (LSPG): $\Psi = \frac{\partial R}{\partial u} \Phi$

Minimum-Residual Property

A ROM possesses the minimum-residual property if $R_r(y, \mu) = 0$ is equivalent to the optimality condition of

$$\min_{oldsymbol{y}\in\mathbb{R}^n} ||oldsymbol{R}(oldsymbol{\Phi}oldsymbol{y}, oldsymbol{\mu})||_{\Theta}$$

for $\Theta \succ 0$

- LSPG possesses minimum-residual property
- Implications
 - Recover exact solution when basis not compressed
 - Monotonic improvement of solution as basis size increases

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Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Nonlinear ROM Bottleneck

• Nonlinear ROM residual and Jacobian:

$$egin{aligned} & m{R}_r(m{y},\ m{\mu}) = m{\Psi}^T m{R}(m{\Phi}m{y},\ m{\mu}) \ & m{\partial}m{R}_r \ & m{\partial}m{y}(m{y},\ m{\mu}) = m{\Psi}^T egin{aligned} & m{\partial}m{R} \ & m{\partial}m{u}(m{\Phi}m{y},\ m{\mu}) m{\Phi} \end{aligned}$$

- Large-scale quantity vs. Small-scale quantity
- To avoid large-scale operations to evaluate residual/Jacobian, introduce **gappy** approximation
 - Only requires evaluation of subset of rows of R and $\frac{\partial R}{\partial u}$
 - ${\scriptstyle \bullet}\,$ In turn only requires subset of rows of Ψ and Φ



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Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Gappy Approximation: Euler Vortex







Gappy Approximation: Euler Vortex





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Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Gappy Approximation: Ahmed Body



(a) 253 sample nodes

(b) 378 sample nodes

(c) 505 sample nodes





Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

ROM-Constrained Optimization

Replace PDE-constrained optimization problem with ROM-constrained optimization problem





Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

ROM-Constrained Optimization

Replace PDE-constrained optimization problem with ROM-constrained optimization problem





Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Offline/Online Approach to ROM-Constrained Optimization





Zahr, Persson, Farhat Optimization/Control Conservation Laws

Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Numerical Experiment: Topology Optimization



Cantilever Schematic



Optimal Solution





Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Numerical Experiment: Topology Optimization





Optimal Solution (HDM)

Optimal Solution (ROM)

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HDM Solution	ROB Construction	Greedy Algorithm	ROM Optimization
$2.84 \times 10^{3} \text{ s}$	$5.48 \times 10^4 \text{ s}$	$1.67 \times 10^{5} { m s}$	30 s
1.26%	24.36%	74.37%	0.01%



HDM Optimization: 1.97×10^4 s



Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Adaptive Approach to ROM-Constrained Optimization





Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Nonlinear Trust-Region Framework

Adaptive Approach to ROM-Constrained Optimization

- $\bullet\,$ Collect snapshots from HDM at $sparse\,\, sampling$ of the parameter space
 - Initial condition for optimization problem
- ${\scriptstyle \bullet}\,$ Build ROB ${\scriptstyle \Phi}\,$ from sparse training
- Solve optimization problem

$$\begin{array}{ll} \underset{\boldsymbol{y} \in \mathbb{R}^{n}, \ \boldsymbol{\mu} \in \mathbb{R}^{p}}{\text{minimize}} & f(\boldsymbol{\Phi}\boldsymbol{y}, \boldsymbol{\mu}) \\ \text{subject to} & \boldsymbol{\Psi}^{T} \boldsymbol{R}(\boldsymbol{\Phi}\boldsymbol{y}, \boldsymbol{\mu}) = 0 \\ & \frac{1}{2} || \boldsymbol{R}(\boldsymbol{\Phi}\boldsymbol{y}, \boldsymbol{\mu}) ||_{2}^{2} \leq \epsilon \end{array}$$

• Use solution of above problem to enrich training and repeat until convergence



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Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Compressible, Inviscid Airfoil Inverse Design





(a) NACA0012: Pressure field $(M_{\infty} = 0.5, \alpha = 0.0^{\circ})$

(b) RAE2822: Pressure field $(M_{\infty} = 0.5, \alpha = 0.0^{\circ})$

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- Pressure discrepancy minimization (Euler equations)
 - Initial Configuration: NACA0012
 - Target Configuration: RAE2822

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Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Optimization Results: How Close?



Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Optimization Results: How Fast?



Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Problem Setup

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- 16000 8-node brick elements, 77760 dofs
- Total Lagrangian form, finite strain, StVK
- St. Venant-Kirchhoff material
- Sparse Cholesky linear solver (CHOLMOD)
- Newton-Raphson nonlinear solver
- Minimum compliance optimization problem



- Gradient computations: Adjoint method
- Optimizer: SNOPT
- Maximum ROM size: $k_{\mathbf{u}} \leq 5$


Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Optimal Solution Comparison



HDM



 $CTRPOD + \Phi_{\mu}$ adaptivity

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HDM Solution	HDM Gradient	HDM Optimization
7458s (450)	4018s (411)	8284s

HDM

Elapsed time = 19761s

HDM Solution	HDM Gradient	ROB Construction	ROM Optimization
1049s~(64)	88s(9)	727s (56)	39s (3676)



 $CTRPOD + \Phi_{\mu}$ adaptivity

Elapsed time = 2197s, Speedup $\approx 9x$



Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Solution after 64 HDM Evaluations



HDM



 $CTRPOD + \Phi_{\mu}$ adaptivity

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- CTRPOD + Φ_{μ} adaptivity: superior approximation to optimal solution than HDM approach after fixed number of HDM solves (64)
- Reasonable option to *warm-start* HDM topology optimization





Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

$CTRPOD + \Phi_{\mu}$ adaptivity





Zahr, Persson, Farhat Optimization/Control Conservation Laws

Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Problem Setup



- $\bullet~64000$ 8-node brick elements, 206715 dofs
- Total Lagrangian formulation, finite strain
- St. Venant-Kirchhoff material
- Jacobi-Preconditioned Conjugate Gradient
- Newton-Raphson nonlinear solver
- Minimum compliance optimization problem

 $\begin{array}{ll} \underset{\mathbf{u}\in\mathbb{R}^{n_{\mathbf{u}}},\ \boldsymbol{\mu}\in\mathbb{R}^{n_{\boldsymbol{\mu}}}}{\text{minimize}} & \mathbf{f}_{\mathrm{ext}}^{T}\mathbf{u} \\ \text{subject to} & V(\boldsymbol{\mu}) \leq 0.15 \cdot V_{0} \\ & \mathbf{r}(\mathbf{u},\ \boldsymbol{\mu}) = 0 \end{array}$

- Gradient computations: Adjoint method
- Optimizer: SNOPT
- Maximum ROM size: $k_{\mathbf{u}} \leq 5$



Shape Optimization: Airfoil Design Minimum Compliance: 2D Cantilever Minimum Compliance: 3D Trestle

Optimal Solution Comparison







 $CTRPOD + \Phi_{\mu}$ adaptivity

- HDM, elapsed time = 179176s
- **CTRPOD**+ Φ_{μ} adaptivity, elapsed time = 15208s



• Speedup $\approx 12 \times$



High-Order Numerical Scheme Fully-Discrete Perturbation Methods Model Order Reduction

Minimum Compliance: 3D Trestle

Solution after 68 HDM Evaluations



 $CTRPOD + \Phi_{\mu}$ adaptivity



- CTRPOD + Φ_{μ} adaptivity: superior approximation to optimal solution than HDM approach after fixed number of HDM solves (68)
- Reasonable option to *warm-start* HDM topology optimization



Conclusion

- Introduced adaptive, nonlinear trust-region framework for accelerating PDE-constrained optimization problems
- Demonstrated approach on canonicals problem from computational mechanics, including nonlinear topology optimization and aerodynamic shape optimization
 - Up to an order of magnitude improvement over standard approach to PDE-constrained optimization
- Next steps: incorporate hyperreduction, 3D, extension to unsteady





- Require mapping $\boldsymbol{x} = \mathcal{G}(\boldsymbol{X}, \boldsymbol{\mu}, t)$ to obtain derivatives $\nabla_{\boldsymbol{X}} \mathcal{G}, \frac{\partial}{\partial t} \mathcal{G}$
- Shape deformation, via Radial Basis Functions (RBFs), applied to reference domain

$$oldsymbol{X}' = oldsymbol{X} + \sum oldsymbol{w}_i \Phi(||oldsymbol{X} - oldsymbol{c}_i||)$$







• Rigid body translation, v, and rotation, Q, applied to deformed configuration

$$X'' = v + QX'$$



Shape Deformation









• Spatial blending between deformation with and without rigid body motion to avoid large velocities at far-field

$$\boldsymbol{x} = b(\boldsymbol{X})\boldsymbol{X}' + (1 - b(\boldsymbol{X}))\boldsymbol{X}''$$

• $b: \mathbb{R}^{n_{sd}} \to \mathbb{R}$ is a function that smoothly transitions from 0 inside a circle of radius R_1 to 1 outside circle of radius R_2















Consistent Discretization of Output Quantities

• Consider any output functional of the form

$$\mathcal{F}(\boldsymbol{U},\boldsymbol{\mu}) = \int_{T_0}^{T_f} \int_{\boldsymbol{\Gamma}} f(\boldsymbol{U},\boldsymbol{\mu},t) \, dS \, dt$$

 \bullet Define f_h as the high-order approximation of the spatial integral via the DG shape functions

$$f_h(\boldsymbol{u}(t),\boldsymbol{\mu},t) = \sum_{\mathcal{T}_e \in \mathcal{T}_{\Gamma}} \sum_{\mathcal{Q}_i \in \mathcal{Q}_{\mathcal{T}_e}} w_i f(\boldsymbol{u}_{ei}(t),\boldsymbol{\mu},t) \approx \int_{\Gamma} f(\boldsymbol{U},\boldsymbol{\mu},t) \, dS$$

• Then, the output functional becomes

$$\mathcal{F}(\boldsymbol{U}, \boldsymbol{\mu}) pprox \mathcal{F}_h(\boldsymbol{u}, \boldsymbol{\mu}) = \int_{T_0}^{T_f} f_h(\boldsymbol{u}(t), \boldsymbol{\mu}, t) \, dt$$



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Consistent Discretization of Output Quantities

• Semi-discretized output functional

$$\mathcal{F}_h(\boldsymbol{u}, \boldsymbol{\mu}, t) = \int_{T_0}^t f_h(\boldsymbol{u}(\tau), \boldsymbol{\mu}, \tau) \, d\tau$$

• Differentiation w.r.t. time leads to

$$\dot{\mathcal{F}}_h(\boldsymbol{u},\boldsymbol{\mu},t) = f_h(\boldsymbol{u}(t),\boldsymbol{\mu},t)$$

• Write semi-discretized output functional *and* conservation law as monolithic system



$$\begin{bmatrix} \mathbf{M} & \mathbf{0} \\ \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \dot{\boldsymbol{u}} \\ \dot{\mathcal{F}}_h \end{bmatrix} = \begin{bmatrix} \boldsymbol{r}(\boldsymbol{u}, \boldsymbol{\mu}, t) \\ f_h(\boldsymbol{u}, \boldsymbol{\mu}, t) \end{bmatrix}$$

• Apply DIRK scheme to obtain

$$\begin{split} \boldsymbol{u}^{(n)} &= \boldsymbol{u}^{(n-1)} + \sum_{i=1}^{s} b_{i} \boldsymbol{k}_{i}^{(n)} \\ \mathcal{F}_{h}^{(n)} &= \mathcal{F}_{h}^{(n-1)} + \sum_{i=1}^{s} b_{i} f_{h} \left(\boldsymbol{u}_{i}^{(n)}, \ \boldsymbol{\mu}, \ t_{i}^{(n-1)} \right) \\ \boldsymbol{u}_{i}^{(n)} &= \boldsymbol{u}^{(n-1)} + \sum_{j=1}^{i} a_{ij} \boldsymbol{k}_{j}^{(n)} \\ \mathbb{M} \boldsymbol{k}_{i}^{(n)} &= \Delta t_{n} \boldsymbol{r} \left(\boldsymbol{u}_{i}^{(n)}, \ \boldsymbol{\mu}, \ t_{i}^{(n-1)} \right) \end{split}$$

where
$$t_i^{(n-1)} = t_{n-1} + c_i \Delta t_n$$

• Only interested in *final* time

$$F(\boldsymbol{u}^{(n)}, \boldsymbol{k}_i^{(n)}, \boldsymbol{\mu}) = \mathcal{F}_h^{(N_t)}$$

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