

Adjoint-Based Optimization of Time-Dependent Fluid-Structure Systems using a High-Order Discontinuous Galerkin Discretization

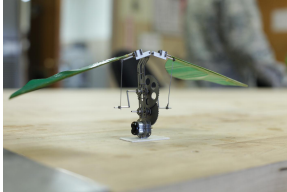
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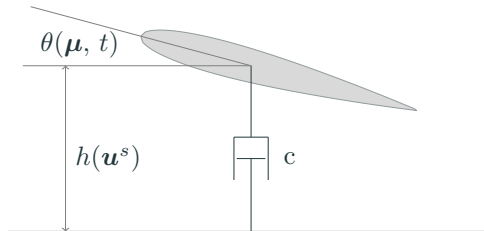
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Optimization of unsteady fluid-structure systems

- Discover energetically optimal **flapping** motions
 - understand biological systems, design Micro Aerial Vehicles (MAVs)



- Design minimal weight structures and vehicles that will not **flutter**
- Design **energy harvesting** mechanisms



Goal: Find the solution of the *unsteady PDE-constrained optimization* problem

$$\begin{aligned} & \underset{\mathbf{U}, \boldsymbol{\mu}}{\text{minimize}} && \mathcal{J}(\mathbf{U}, \boldsymbol{\mu}) \\ & \text{subject to} && \mathbf{C}(\mathbf{U}, \boldsymbol{\mu}) \leq 0 \\ & && \frac{\partial \mathbf{U}}{\partial t} + \nabla \cdot \mathbf{F}(\mathbf{U}, \nabla \mathbf{U}) = 0 \quad \text{in } v(\boldsymbol{\mu}, t) \end{aligned}$$

where

- $\mathbf{U}(\mathbf{x}, t)$ PDE solution
- $\boldsymbol{\mu}$ design/control parameters
- $\mathcal{J}(\mathbf{U}, \boldsymbol{\mu}) = \int_{T_0}^{T_f} \int_{\Gamma} j(\mathbf{U}, \boldsymbol{\mu}, t) dS dt$ objective function
- $\mathbf{C}(\mathbf{U}, \boldsymbol{\mu}) = \int_{T_0}^{T_f} \int_{\Gamma} \mathbf{c}(\mathbf{U}, \boldsymbol{\mu}, t) dS dt$ constraints



- *Continuous* PDE-constrained optimization problem

$$\begin{aligned} & \underset{\mathbf{U}, \boldsymbol{\mu}}{\text{minimize}} && \mathcal{J}(\mathbf{U}, \boldsymbol{\mu}) \\ & \text{subject to} && \mathbf{C}(\mathbf{U}, \boldsymbol{\mu}) \leq 0 \\ & && \frac{\partial \mathbf{U}}{\partial t} + \nabla \cdot \mathbf{F}(\mathbf{U}, \nabla \mathbf{U}) = 0 \quad \text{in } v(\boldsymbol{\mu}, t) \end{aligned}$$

- *Fully discrete* PDE-constrained optimization problem

$$\begin{aligned} & \underset{\substack{\mathbf{u}_0, \dots, \mathbf{u}_{N_t} \in \mathbb{R}^{N_u}, \\ \mathbf{k}_{1,1}, \dots, \mathbf{k}_{N_t,s} \in \mathbb{R}^{N_u}, \\ \boldsymbol{\mu} \in \mathbb{R}^{n_\mu}}}{\text{minimize}} && J(\mathbf{u}_0, \dots, \mathbf{u}_{N_t}, \mathbf{k}_{1,1}, \dots, \mathbf{k}_{N_t,s}, \boldsymbol{\mu}) \\ & \text{subject to} && \mathbf{C}(\mathbf{u}_0, \dots, \mathbf{u}_{N_t}, \mathbf{k}_{1,1}, \dots, \mathbf{k}_{N_t,s}, \boldsymbol{\mu}) \leq 0 \\ & && \mathbf{u}_0 - \mathbf{g}(\boldsymbol{\mu}) = 0 \\ & && \mathbf{u}_n - \mathbf{u}_{n-1} - \sum_{i=1}^s b_i \mathbf{k}_{n,i} = 0 \\ & && \mathbf{M} \mathbf{k}_{n,i} - \Delta t_n \mathbf{r}(\mathbf{u}_{n,i}, \boldsymbol{\mu}, t_{n,i}) = 0 \end{aligned}$$



Highlights of globally high-order discretization

- **Arbitrary Lagrangian-Eulerian** formulation:
Map, $\mathcal{G}(\cdot, \boldsymbol{\mu}, t)$, from physical $v(\boldsymbol{\mu}, t)$ to reference V

$$\left. \frac{\partial \mathbf{U}_X}{\partial t} \right|_X + \nabla_X \cdot \mathbf{F}_X(\mathbf{U}_X, \nabla_X \mathbf{U}_X) = 0$$

- **Space discretization:** discontinuous Galerkin

$$M \frac{\partial \mathbf{u}}{\partial t} = \mathbf{r}(\mathbf{u}, \boldsymbol{\mu}, t)$$

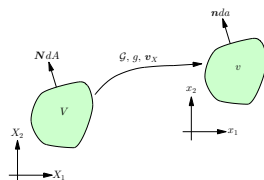
- **Time discretization:** diagonally implicit RK

$$\mathbf{u}_n = \mathbf{u}_{n-1} + \sum_{i=1}^s b_i \mathbf{k}_{n,i}$$

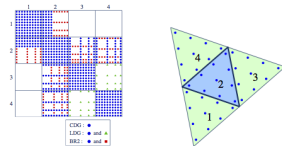
$$M \mathbf{k}_{n,i} = \Delta t_n \mathbf{r}(\mathbf{u}_{n,i}, \boldsymbol{\mu}, t_{n,i})$$

- **Quantity of interest:** solver-consistency

$$F(\mathbf{u}_0, \dots, \mathbf{u}_{N_t}, \mathbf{k}_{1,1}, \dots, \mathbf{k}_{N_t,s})$$



Mapping-Based ALE



DG Discretization

c_1	a_{11}			
c_2	a_{21}	a_{22}		
\vdots	\vdots	\vdots	\ddots	
c_s	a_{s1}	a_{s2}	\cdots	a_{ss}
	b_1	b_2	\cdots	b_s

Butcher Tableau for DIRK

- Consider the *fully discrete* output functional $F(\mathbf{u}_n, \mathbf{k}_{n,i}, \boldsymbol{\mu})$
 - Represents either the **objective** function or a **constraint**
- The *total derivative* with respect to the parameters $\boldsymbol{\mu}$, required in the context of gradient-based optimization, takes the form

$$\frac{dF}{d\boldsymbol{\mu}} = \frac{\partial F}{\partial \boldsymbol{\mu}} + \sum_{n=0}^{N_t} \frac{\partial F}{\partial \mathbf{u}_n} \frac{\partial \mathbf{u}_n}{\partial \boldsymbol{\mu}} + \sum_{n=1}^{N_t} \sum_{i=1}^s \frac{\partial F}{\partial \mathbf{k}_{n,i}} \frac{\partial \mathbf{k}_{n,i}}{\partial \boldsymbol{\mu}}$$

- The sensitivities, $\frac{\partial \mathbf{u}_n}{\partial \boldsymbol{\mu}}$ and $\frac{\partial \mathbf{k}_{n,i}}{\partial \boldsymbol{\mu}}$, are expensive to compute, requiring the solution of $n_{\boldsymbol{\mu}}$ linear evolution equations
- **Adjoint method**: alternative method for computing $\frac{dF}{d\boldsymbol{\mu}}$ that require one linear evolution equation for each quantity of interest, F



Adjoint equation derivation: outline

- Define **auxiliary** PDE-constrained optimization problem

$$\begin{aligned} & \text{minimize} && F(\mathbf{u}_0, \dots, \mathbf{u}_{N_t}, \mathbf{k}_{1,1}, \dots, \mathbf{k}_{N_t,s}, \boldsymbol{\mu}) \\ & \mathbf{u}_0, \dots, \mathbf{u}_{N_t} \in \mathbb{R}^{N_u}, \\ & \mathbf{k}_{1,1}, \dots, \mathbf{k}_{N_t,s} \in \mathbb{R}^{N_u} \end{aligned}$$

$$\text{subject to} \quad \mathbf{R}_0 = \mathbf{u}_0 - \mathbf{g}(\boldsymbol{\mu}) = 0$$

$$\mathbf{R}_n = \mathbf{u}_n - \mathbf{u}_{n-1} - \sum_{i=1}^s b_i \mathbf{k}_{n,i} = 0$$

$$\mathbf{R}_{n,i} = M \mathbf{k}_{n,i} - \Delta t_n \mathbf{r}(\mathbf{u}_{n,i}, \boldsymbol{\mu}, t_{n,i}) = 0$$

- Define **Lagrangian**

$$\mathcal{L}(\mathbf{u}_n, \mathbf{k}_{n,i}, \boldsymbol{\lambda}_n, \boldsymbol{\kappa}_{n,i}) = F - \boldsymbol{\lambda}_0^T \mathbf{R}_0 - \sum_{n=1}^{N_t} \boldsymbol{\lambda}_n^T \mathbf{R}_n - \sum_{n=1}^{N_t} \sum_{i=1}^s \boldsymbol{\kappa}_{n,i}^T \mathbf{R}_{n,i}$$

- The solution of the optimization problem is given by the **Karush-Kuhn-Tucker (KKT)** system

$$\frac{\partial \mathcal{L}}{\partial \mathbf{u}_n} = 0, \quad \frac{\partial \mathcal{L}}{\partial \mathbf{k}_{n,i}} = 0, \quad \frac{\partial \mathcal{L}}{\partial \boldsymbol{\lambda}_n} = 0, \quad \frac{\partial \mathcal{L}}{\partial \boldsymbol{\kappa}_{n,i}} = 0$$



Dissection of fully discrete adjoint equations

- **Linear** evolution equations solved **backward** in time
- **Primal** state/stage, $\mathbf{u}_{n,i}$ required at each state/stage of dual problem
- Heavily dependent on **chosen output**

$$\lambda_{N_t} = \frac{\partial F}{\partial \mathbf{u}_{N_t}}^T$$

$$\lambda_{n-1} = \lambda_n + \frac{\partial F}{\partial \mathbf{u}_{n-1}}^T + \sum_{i=1}^s \Delta t_n \frac{\partial \mathbf{r}}{\partial \mathbf{u}}(\mathbf{u}_{n,i}, \boldsymbol{\mu}, t_{n-1} + c_i \Delta t_n)^T \boldsymbol{\kappa}_{n,i}$$

$$M^T \boldsymbol{\kappa}_{n,i} = \frac{\partial F}{\partial \mathbf{u}_{N_t}}^T + b_i \lambda_n + \sum_{j=i}^s a_{ji} \Delta t_n \frac{\partial \mathbf{r}}{\partial \mathbf{u}}(\mathbf{u}_{n,j}, \boldsymbol{\mu}, t_{n-1} + c_j \Delta t_n)^T \boldsymbol{\kappa}_{n,j}$$

- Gradient reconstruction via dual variables

$$\frac{dF}{d\boldsymbol{\mu}} = \frac{\partial F}{\partial \boldsymbol{\mu}} + \lambda_0^T \frac{\partial \mathbf{g}}{\partial \boldsymbol{\mu}}(\boldsymbol{\mu}) + \sum_{n=1}^{N_t} \Delta t_n \sum_{i=1}^s \boldsymbol{\kappa}_{n,i}^T \frac{\partial \mathbf{r}}{\partial \boldsymbol{\mu}}(\mathbf{u}_{n,i}, \boldsymbol{\mu}, t_{n,i})$$

[Zahr and Persson, 2016]



Energetically optimal flapping vs. required thrust

Energy = 0.21935

Thrust = 0.0000

Energy = 3.00404

Thrust = 1.5000

Energy = 6.2869

Thrust = 2.5000

Optimal $T_x = 0$

Optimal
 $T_x = 1.5$

Optimal
 $T_x = 2.5$



Structure: semi-discretization, first-order form

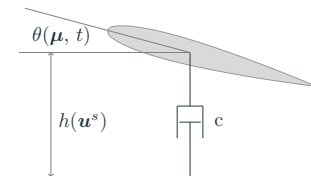
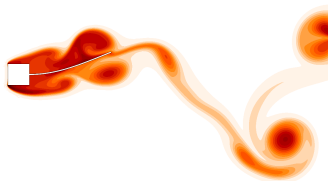
$$M^s \frac{\partial \mathbf{u}^s}{\partial t} = \mathbf{r}^s(\mathbf{u}^s; \mathbf{t}) = \mathbf{r}^{ss}(\mathbf{u}^s) + \mathbf{r}^{sf} \cdot \mathbf{t}$$

- Semidiscretization (CG-FEM) of **continuum** (hyperelasticity)

$$\begin{aligned} \frac{\partial \mathbf{p}}{\partial t} - \nabla \cdot \mathbf{P}(\mathbf{G}) &= \mathbf{b} && \text{in } \Omega_0 \\ \mathbf{P}(\mathbf{G}) \cdot \mathbf{N} &= \mathbf{t} && \text{on } \Gamma_N \\ \mathbf{x} &= \mathbf{x}_D && \text{on } \Gamma_D \end{aligned}$$

- Force balance on **rigid body**

$$M \frac{\partial^2 \mathbf{q}}{\partial t^2} + C \frac{\partial \mathbf{q}}{\partial t} + \mathbf{K} \mathbf{q} = \mathbf{t}$$



Coupled fluid-structure formulation

- Write discretized fluid and structure equations as ODEs

$$M^f \dot{\mathbf{u}}^f = \mathbf{r}^f(\mathbf{u}^f; \mathbf{x})$$

$$\begin{aligned} M^s \dot{\mathbf{u}}^s &= \mathbf{r}^s(\mathbf{u}^s; \mathbf{t}) \\ &= \mathbf{r}^{ss}(\mathbf{u}^s) + \mathbf{r}^{sf} \cdot \mathbf{t} \end{aligned}$$

in the fluid \mathbf{u}^f and structure \mathbf{u}^s variables

- Apply couplings
 - Structure-to-fluid: deform fluid domain $\mathbf{x} = \mathbf{x}(\mathbf{u}^s)$
 - Fluid-to-structure: apply boundary traction $\mathbf{t} = \mathbf{t}(\mathbf{u}^f)$
- Write coupled system as $M\dot{\mathbf{u}} = \mathbf{r}(\mathbf{u})$

$$\mathbf{u} = \begin{bmatrix} \mathbf{u}^f \\ \mathbf{u}^s \end{bmatrix} \quad \mathbf{r}(\mathbf{u}) = \begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \mathbf{t}(\mathbf{u}^f)) \end{bmatrix} \quad M = \begin{bmatrix} M^f & \\ & M^s \end{bmatrix}$$



High-order partitioned FSI solver: IMEX Runge-Kutta¹

- Exploit **linear dependence** of structure residual (\mathbf{r}^s) on traction (\mathbf{t})

$$\mathbf{r}(\mathbf{u}) = \begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \mathbf{t}(\mathbf{u}^f)) \end{bmatrix} = \underbrace{\begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^{sf} \cdot (\mathbf{t}(\mathbf{u}^f) - \tilde{\mathbf{t}}) \end{bmatrix}}_{\mathbf{f}(\mathbf{u})} + \underbrace{\begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \tilde{\mathbf{t}}) \end{bmatrix}}_{\mathbf{g}(\mathbf{u})}$$

- Apply **high-order** implicit-explicit Runge-Kutta scheme to discretize

$$M \frac{\partial \mathbf{u}}{\partial t} = \mathbf{r}(\mathbf{u}) = \underbrace{\mathbf{f}(\mathbf{u})}_{\text{explicit}} + \underbrace{\mathbf{g}(\mathbf{u})}_{\text{implicit}}$$

- Explicit Runge-Kutta scheme \hat{c} , \hat{A} , \hat{b} for $\mathbf{f}(\mathbf{u})$
- Diagonally implicit scheme c , A , b for $\mathbf{g}(\mathbf{u})$

$$\mathbf{u}_n = \mathbf{u}_{n-1} + \sum_{i=1}^s \hat{b}_i \hat{\mathbf{k}}_{n,i} + \sum_{i=1}^s b_i \mathbf{k}_{n,i}$$

$$M \mathbf{k}_{n,i} = \Delta t_n \mathbf{g} \left(\mathbf{u}_{n-1} + \sum_{j=1}^{i-1} \hat{a}_{ij} \hat{\mathbf{k}}_{n,j} + \sum_{j=1}^i a_{ij} \mathbf{k}_{n,j} \right)$$

$$M \hat{\mathbf{k}}_{n,i} = \Delta t_n \mathbf{f} \left(\mathbf{u}_{n-1} + \sum_{j=1}^{i-1} \hat{a}_{ij} \hat{\mathbf{k}}_{n,j} + \sum_{j=1}^i a_{ij} \mathbf{k}_{n,j} \right)$$

¹[van Zuijlen and Bijl, 2005, Froehle and Persson, 2014]

High-order partitioned FSI solver: IMEX Runge-Kutta¹

- Exploit **linear dependence** of structure residual (\mathbf{r}^s) on traction (\mathbf{t})

$$\mathbf{r}(\mathbf{u}) = \begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \mathbf{t}(\mathbf{u}^f)) \end{bmatrix} = \underbrace{\begin{bmatrix} \mathbf{r}^{sf} \cdot (\mathbf{t}(\mathbf{u}^f) - \tilde{\mathbf{t}}) \end{bmatrix}}_{f(\mathbf{u})} + \underbrace{\begin{bmatrix} \mathbf{r}^f(\mathbf{u}^f; \mathbf{x}(\mathbf{u}^s)) \\ \mathbf{r}^s(\mathbf{u}^s; \tilde{\mathbf{t}}) \end{bmatrix}}_{g(\mathbf{u})}$$

- Solve: (1) implicit **structure**, (2) implicit **fluid**, (3) explicit **structure**
- Due to choice of IMEX partition: **no explicit fluid stages**

¹[van Zuijlen and Bijl, 2005, Froehle and Persson, 2014]

- Define stage solutions

$$\mathbf{u}_{n,i}^s = \mathbf{u}_{n-1}^s + \sum_{j=1}^i a_{ij} \mathbf{k}_{n,j}^s + \sum_{j=1}^{i-1} \hat{a}_{ij} \hat{\mathbf{k}}_{n,j}^s$$

$$\mathbf{u}_{n,i}^f = \mathbf{u}_{n-1}^f + \sum_{j=1}^i a_{ij} \mathbf{k}_{n,j}^f$$

- Define **traction predictor** as true traction at previous stage

$$\tilde{\mathbf{t}}_{n,i} = \mathbf{t}(\mathbf{u}_{n,i-1})$$

- Solve for **stage velocities** ($i = 1, \dots, s$)

$$M^s \mathbf{k}_{n,i}^s = \Delta t_n \mathbf{r}^s(\mathbf{u}_{n,i}^s; \tilde{\mathbf{t}}_{n,i})$$

$$M^f \mathbf{k}_{n,i}^f = \Delta t_n \mathbf{r}^f(\mathbf{u}_{n,i}^f; \mathbf{x}(\mathbf{u}_{n,i}^s))$$

$$M^s \hat{\mathbf{k}}_{n,i}^s = \Delta t_n \mathbf{r}^{sf}(\mathbf{t}(\mathbf{u}_{n,i}^f) - \tilde{\mathbf{t}}_{n,i})$$

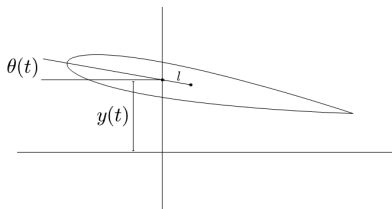
- Update state solution at new time

$$\mathbf{u}_n^f = \mathbf{u}_{n-1}^f + \sum_{j=1}^s b_j \mathbf{k}_{n,j}^f, \quad \mathbf{u}_n^s = \mathbf{u}_{n-1}^s + \sum_{j=1}^s b_j \mathbf{k}_{n,j}^s + \sum_{j=1}^s \hat{b}_j \hat{\mathbf{k}}_{n,j}^s$$



Validation: benchmark pitching airfoil system

- Simple FSI benchmark problem for studying the high-order accuracy of the IMEX scheme
- Rigid pitching/heaving NACA 0012 airfoil, torsional spring
- Smooth heaving step $y(t)$ prescribed, angle $\theta(t)$ measured



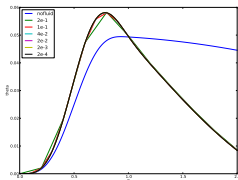
Setup

Mach number

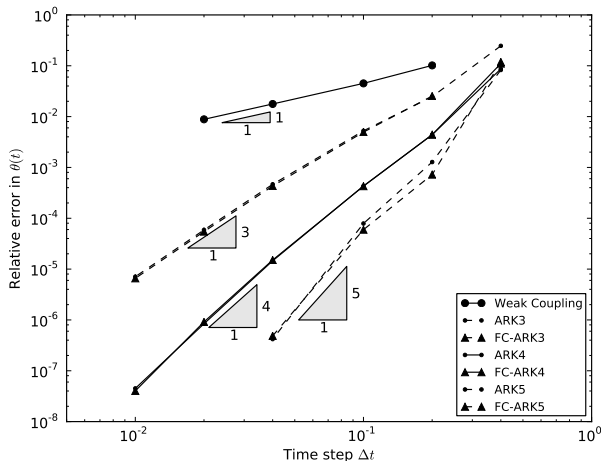


Validation: benchmark pitching airfoil system

- Up to 5th order of convergence in time.
- Similar accuracy as solving fully coupled system



Angle $\theta(t)$ vs time t

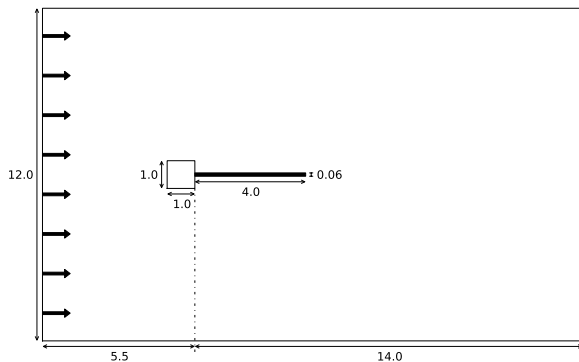


Entropy



Validation: cantilever system

- Standard FSI benchmark problem.
- Elastic cantilever behind a square bluff body in incompressible flow.



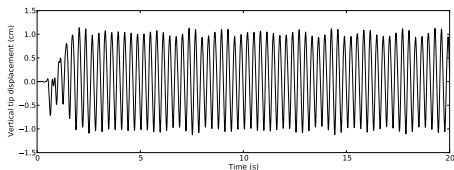
- Cantilever:
 $\rho_s = 100 \text{ kg/m}^3$, $\nu_s = 0.35$,
 $E = 2.5 \times 10^5 \text{ Pa}$.
- Fluid & Flow:
 $\rho_f = 1.18 \text{ kg/m}^3$,
 $\nu_f = 1.54 \times 10^{-5} \text{ m}^2/\text{s}$,
 $v_f = 0.513 \text{ m/s}$, $\text{Re} = 333$,
 $\text{Ma} = 0.2$.

- Vortex shedding frequency: $\sim 6.3 \text{ Hz}$
Cantilever first mode: 3.03 Hz



Validation: cantilever system

Entropy



- Tip frequency:
 $f = 3.14 \text{ Hz}$
(Literature:
2.98 – 3.25 Hz)
- Tip displacement:
 $d_{max} = 1.09 \text{ cm}$
(Literature:
0.95 – 1.25 cm)



Flow around Membrane, 3-D

- Angle of attack 22.6° , Reynolds number 2000.
- Flexible structure prevents leading edge separation.



Adjoint equations for high-order partitioned IMEX FSI solver

- Define

$$\mathbf{r}_{n,i}^f = \mathbf{r}^f(\mathbf{u}_{n,i}^f; \mathbf{x}(\mathbf{u}_{n,i}^s)) \quad \mathbf{r}_{n,i}^s = \mathbf{r}^s(\mathbf{u}_{n,i}^s; \tilde{\mathbf{t}}_{n,i})$$

- **Final condition** for state Lagrange multipliers (F is quantity of interest)

$$\boldsymbol{\lambda}_{N_t}^f = \frac{\partial F}{\partial \mathbf{u}_{N_t}^f}{}^T, \quad \boldsymbol{\lambda}_{N_t}^s = \frac{\partial F}{\partial \mathbf{u}_{N_t}^s}{}^T$$

- Solve for **stage** Lagrange multipliers ($j = s, \dots, 1$)

- **Explicit structure stage**

$$\mathbf{M}^{sT} \hat{\boldsymbol{\kappa}}_{n,j}^s = \frac{\partial F}{\partial \hat{\mathbf{k}}_{n,j}^s}{}^T + \hat{b}_j \boldsymbol{\lambda}_n^s + \Delta t_n \sum_{i=j+1}^s \hat{a}_{ij} \frac{\partial \mathbf{r}_{n,i}^f}{\partial \mathbf{u}^s}{}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=j+1}^s \hat{a}_{ij} \frac{\partial \mathbf{r}_{n,i}^s}{\partial \mathbf{u}^s}{}^T \boldsymbol{\kappa}_{n,i}^s$$

- **Implicit fluid stage**

$$\begin{aligned} \mathbf{M}^{fT} \boldsymbol{\kappa}_{n,j}^f &= \frac{\partial F}{\partial \mathbf{k}_{n,j}^f}{}^T + b_j \boldsymbol{\lambda}_n^f + \Delta t_n \sum_{i=j}^s a_{ij} \frac{\partial \mathbf{r}_{n,i}^f}{\partial \mathbf{u}^f}{}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=j+1}^s a_{ij} \frac{\partial \tilde{\mathbf{t}}_{n,i}}{\partial \mathbf{u}^f}{}^T \mathbf{r}^{sfT} \boldsymbol{\kappa}_{n,i}^s \\ &\quad - \Delta t_n \sum_{i=j}^s a_{ij} \frac{\partial \mathbf{t}_{n,i}}{\partial \mathbf{u}^f}{}^T \mathbf{r}^{sfT} \hat{\boldsymbol{\kappa}}_{n,i}^s + \Delta t_n \sum_{i=j+1}^s a_{ij} \frac{\partial \tilde{\mathbf{t}}_{n,i}}{\partial \mathbf{u}^f}{}^T \mathbf{r}^{sfT} \hat{\boldsymbol{\kappa}}_{n,i}^s \end{aligned}$$

- **Implicit structure stage**

$$\mathbf{M}^{sT} \boldsymbol{\kappa}_{n,j}^s = \frac{\partial F}{\partial \mathbf{k}_{n,j}^s}{}^T + b_j \boldsymbol{\lambda}_n^s + \Delta t_n \sum_{i=j}^s a_{ij} \frac{\partial \mathbf{r}_{n,i}^f}{\partial \mathbf{u}^s}{}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=j}^s a_{ij} \frac{\partial \mathbf{r}_{n,i}^s}{\partial \mathbf{u}^s}{}^T \boldsymbol{\kappa}_{n,i}^s$$

- Update state Lagrange multipliers at new time

$$\begin{aligned} \lambda_{n-1}^f = \lambda_n^f + \frac{\partial F}{\partial \mathbf{u}_{n-1}^f}{}^T + \Delta t_n \sum_{i=1}^s \frac{\partial \mathbf{r}_{n,i}^f}{\partial \mathbf{u}^f}{}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=1}^s \frac{\partial \tilde{\mathbf{t}}_{n,i}}{\partial \mathbf{u}^f}{}^T \mathbf{r}_{n,i}^{sf}{}^T \boldsymbol{\kappa}_{n,i}^s \\ + \Delta t_n \sum_{i=1}^s \left[\frac{\partial \tilde{\mathbf{t}}_{n,i}}{\partial \mathbf{u}^f} - \frac{\partial \mathbf{t}_{n,i}}{\partial \mathbf{u}^f} \right]{}^T \mathbf{r}_{n,i}^{sf}{}^T \hat{\boldsymbol{\kappa}}_{n,i}^s \end{aligned}$$

$$\lambda_{n-1}^s = \lambda_n^s + \frac{\partial F}{\partial \mathbf{u}_{n-1}^s}{}^T + \Delta t_n \sum_{i=1}^s \frac{\partial \mathbf{r}_{n,i}^f}{\partial \mathbf{u}^s}{}^T \boldsymbol{\kappa}_{n,i}^f + \Delta t_n \sum_{i=1}^s \frac{\partial \mathbf{r}_{n,i}^s}{\partial \mathbf{u}^s}{}^T \boldsymbol{\kappa}_{n,i}^s$$

- Reconstruct **total derivative** of quantity of interest F as

$$\begin{aligned} \frac{dF}{d\boldsymbol{\mu}} = \frac{\partial F}{\partial \boldsymbol{\mu}} + \boldsymbol{\lambda}_0^f{}^T \frac{\partial \bar{\mathbf{u}}^f}{\partial \boldsymbol{\mu}} + \boldsymbol{\lambda}_0^s{}^T \frac{\partial \bar{\mathbf{u}}^s}{\partial \boldsymbol{\mu}} - \sum_{n=0}^{N_t} \Delta t_n \sum_{i=1}^s \boldsymbol{\kappa}_{n,i}^f{}^T \frac{\partial \mathbf{r}_{n,i}^f}{\partial \boldsymbol{\mu}} \\ - \sum_{n=0}^{N_t} \Delta t_n \sum_{i=1}^s \boldsymbol{\kappa}_{n,i}^s{}^T \frac{\partial \mathbf{r}_{n,i}^s}{\partial \boldsymbol{\mu}} - \sum_{n=0}^{N_t} \Delta t_n \sum_{i=1}^s \hat{\boldsymbol{\kappa}}_{n,i}^{s,T} \frac{\partial \mathbf{r}_{n,i}^{sf}}{\partial \boldsymbol{\mu}} \end{aligned}$$

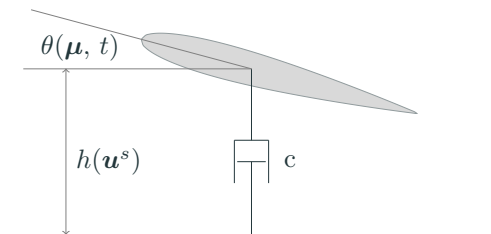


Optimal energy harvesting from foil-damper system

Goal: Maximize energy harvested from foil-damper system

$$\underset{\boldsymbol{\mu}}{\text{maximize}} \quad \frac{1}{T} \int_0^T (c\dot{h}^2(\mathbf{u}^s) - M_z(\mathbf{u}^f)\dot{\theta}(\boldsymbol{\mu}, t)) dt$$

- Fluid: Isentropic Navier-Stokes on deforming domain (ALE)
- Structure: Force balance in y -direction between foil and damper
- Motion driven by *imposed* $\theta(\boldsymbol{\mu}, t) = \mu_1 \cos(2\pi ft)$







$$\mu_1^* \approx 45^\circ$$




Summary

- Extended standard fully discrete adjoint framework to partitioned, high-order multiphysics setting
- Demonstrated on simple optimal energy harvesting model problem

Future work

- Extend structure model to fully deformable model
 - High-order, energy conserving load transfer from fluid to structure
 - Handle discontinuities between fluid elements that arise from DG discretization
- Study optimal 3D flapping with deformable wing

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